



Simulation SMR-NuScale with PARCS code

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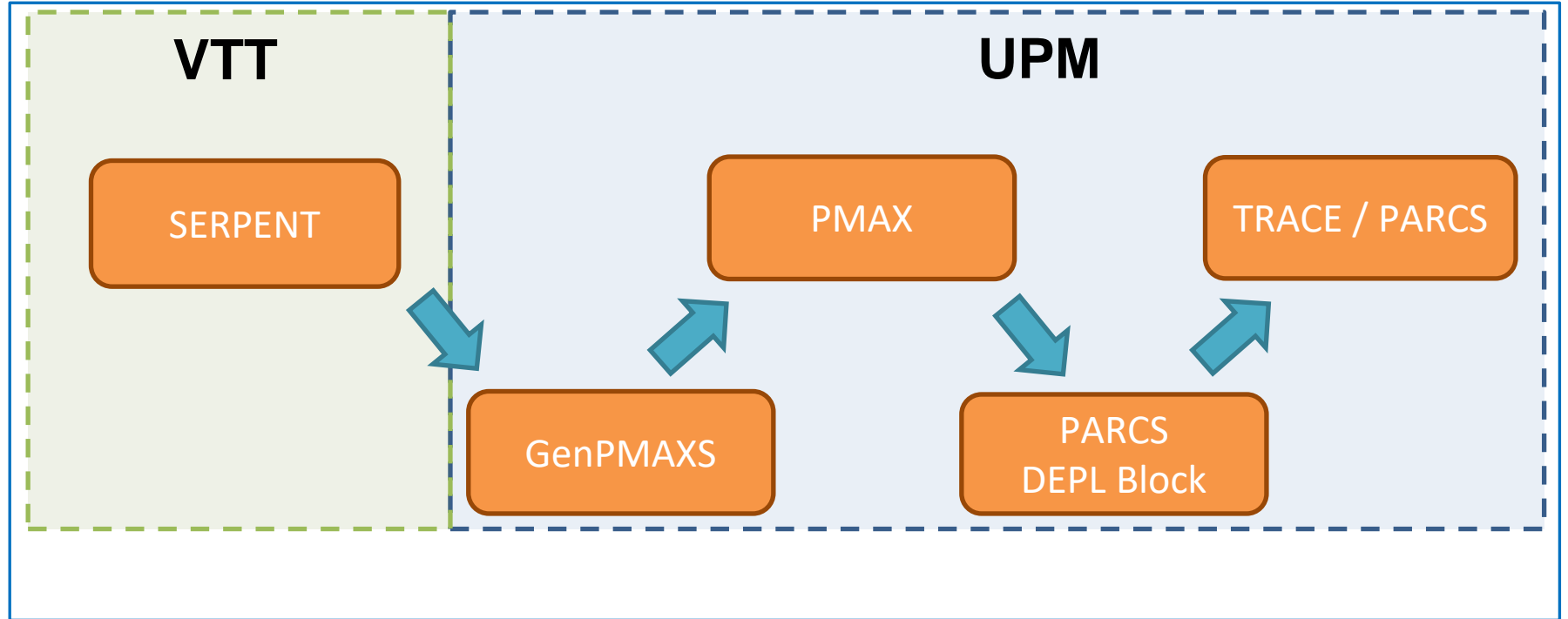
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UPM

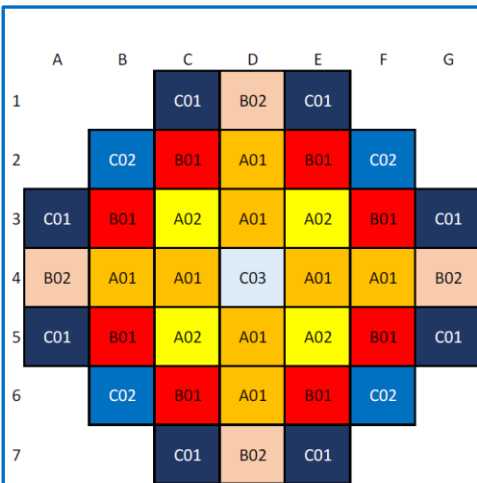
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NuScale Core



A01	1.50 wt% U235
A02	1.60 wt% U235
B01	2.50 wt% U235
B02	2.60 wt% U235
C01	4.05 wt% U235
C02	4.55 wt% U235 + 16 pins Gd2O3
C03	2.60 wt% U235

Core thermal output	160MWth
System pressure	1850 psia
Inlet temperature	258.3 °C
Core average temperature	283.9 °C
Fuel assemblies	37 (17x17)
Diameter active core	150.57 cm

Partial CRs	AgInCd (30.48cm) + B4C (157.48 cm)
Fuel rod pitch (cold)	1.2598 cm
Fuel assembly pitch	21.5036 cm
Active height	200 cm



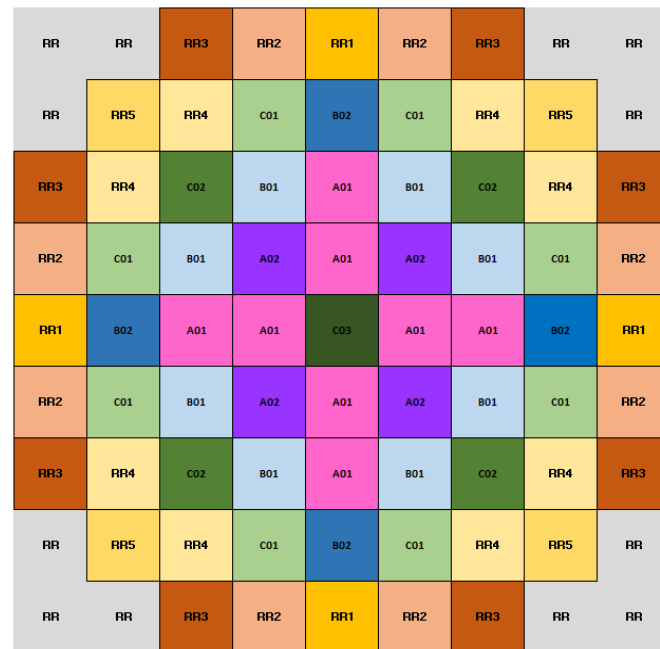
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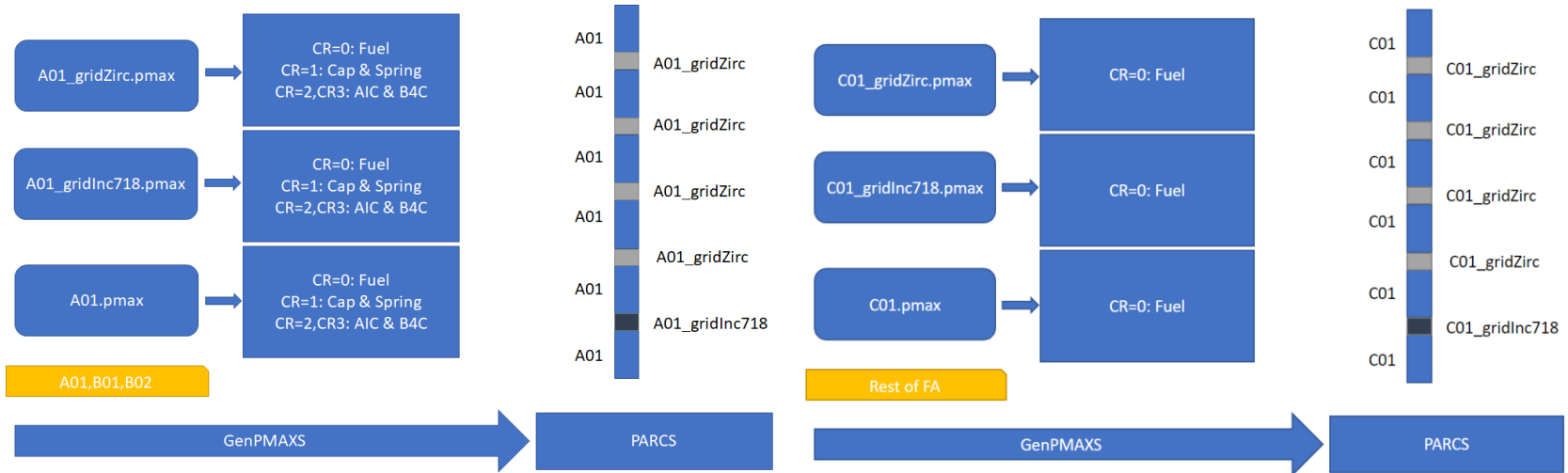
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- The XS have been provided by VTT.
- Fresh fuel (at **zero burnup**) is considered.
- **Four energy groups.**
- ENDF/B-VII.1. library has been used.

STATE VARIABLES	BRANCHING
DM (g/cm ³)	0.9, 0.8, 0.7, 0.6, 0.5, 0.3
PM (ppm)	0, 1000, 2000
TF (K)	900

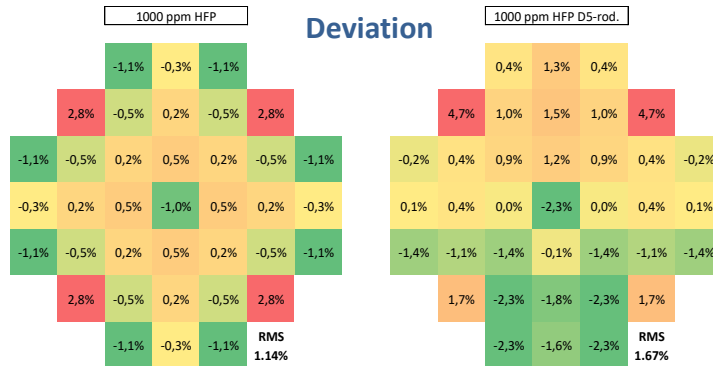


GenPMAXS allows to treat CRs with different absorber materials.
CR, TF, PC and DC state variables are allowed.

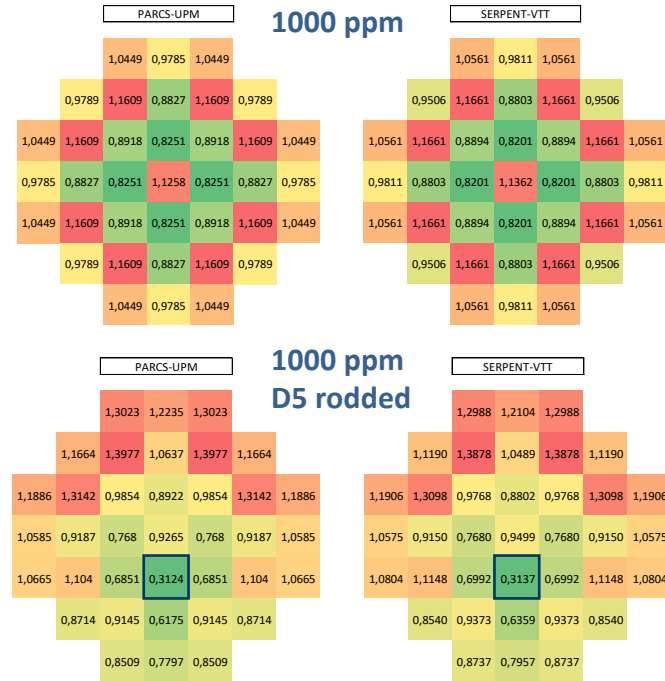


SERPENT vs. PARCS Benchmark. Radial Power Distribution at BOC

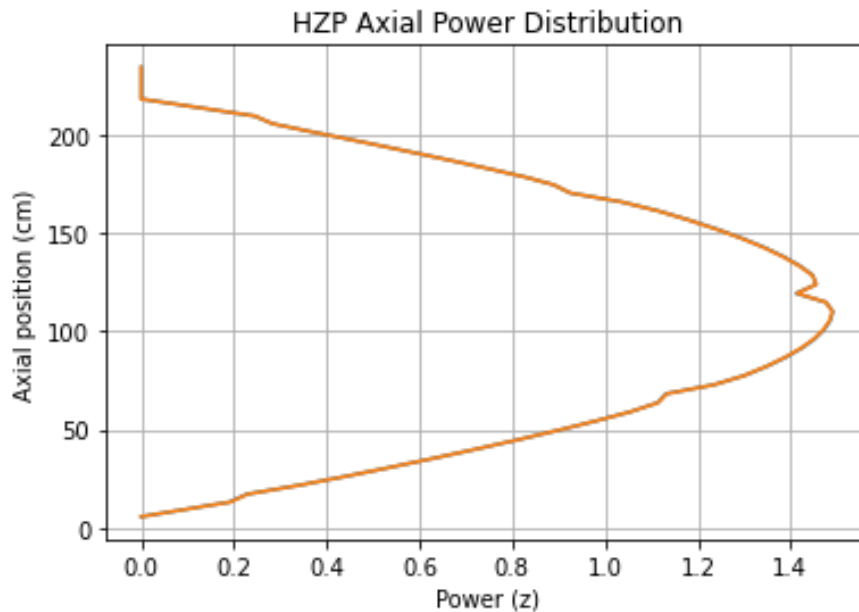
Keff (HFP)	PARCS	SERPENT
1000 ppm	1.02845	1.02762
1000 ppm, D5 rodded	1.02223	1.02207



NEMMG has been employed.



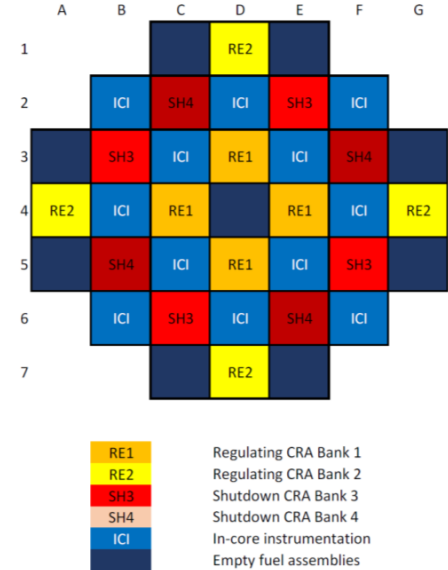
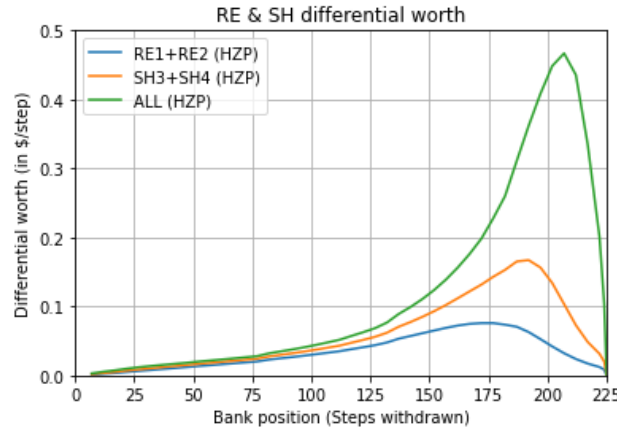
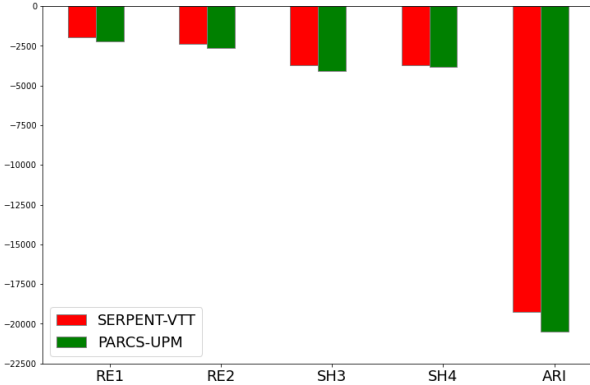
Axial Power Distribution at BOC



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Control Rod Worth

CRW, pcm

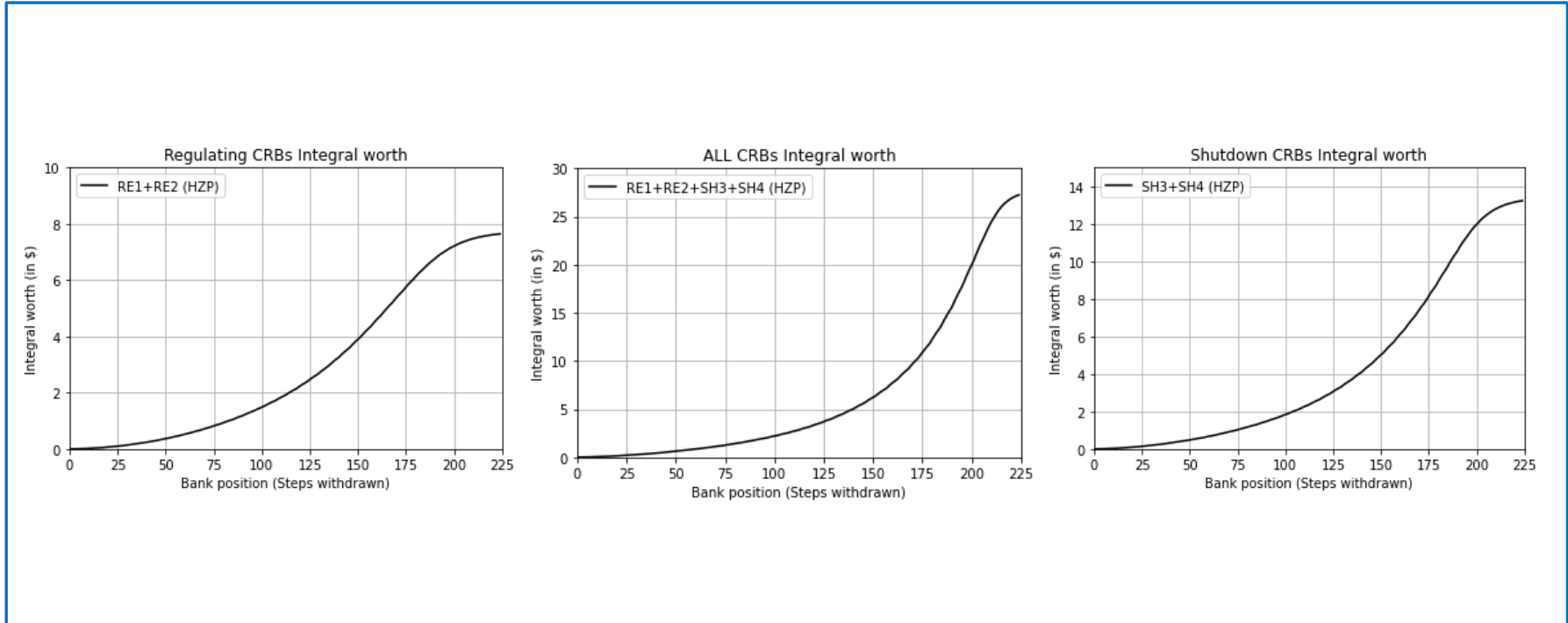


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Integral CRs Worth

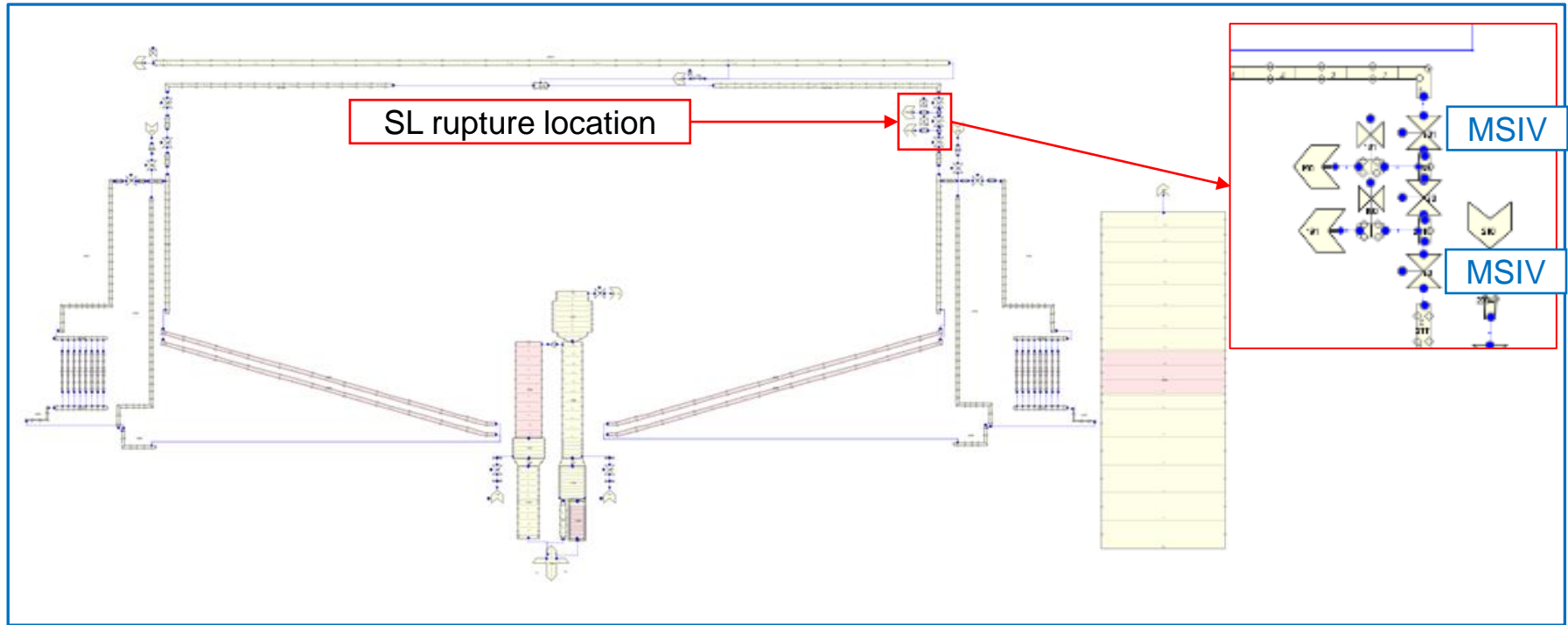


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TRACE 1D model. Steam Line Break. Nodalization scheme



TRACE 1D model. Steam Line Break. McSAFER hypotheses

Initial conditions:

Parameter	Nominal Value	DEGB-SL
Core Power (MWt)	160	100% (IC fixed)
Rupture Location	-	SL between the primary and secondary MSIVs
PZR Pressure (MPa)	12.755	12.755
Pressurizer Level (%)	60	60
RCS Flow rate (kg/s)	544.29	535 (IC fixed)
RCS Avg. Temp. (K)	558.15	563.71
SG Pressure (MPa)	3.447	3.689
Core exposure		Burn-up = 0.0

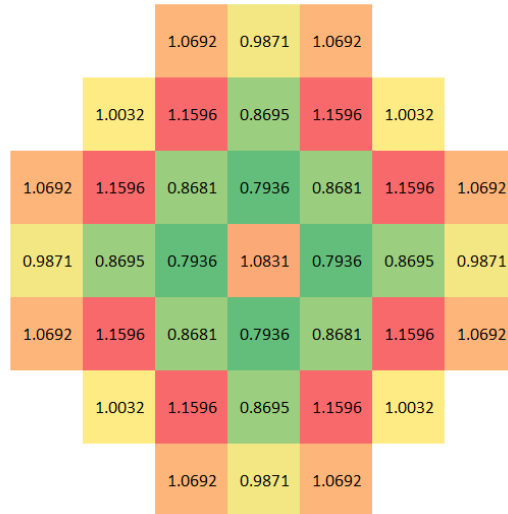
Hypotheses McSAFER:

- Initial power level is assumed to be **100 % RTP** at BOC condition along with **high RCS temperature** and **SG pressure**.
- The **Low Steam Pressure Trip** signal is **credited**.
- The **High Core Power Trip** signal is **credited (125%)**.
- It is assumed that **normal AC power is available**.
- The **failure of the primary MSIV** associated with the impacted SG train is assumed.
- The **FW flow is allowed to be increased** in **0.181 kg/s** for every **0.00689 MPa** decrease in SG pressure.

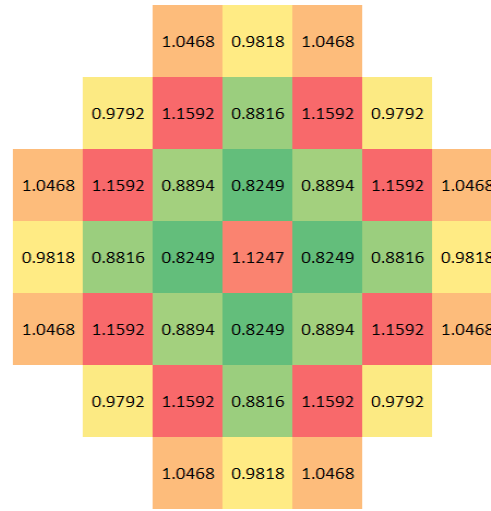


TRACE-1D/PARCS-3D model. Steady-State Power Distribution

Radial Power Distribution

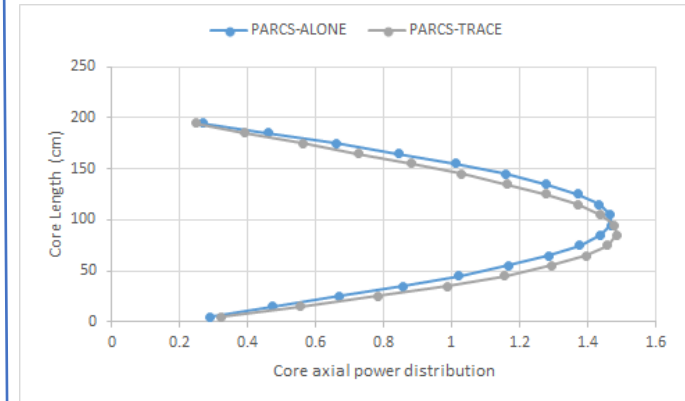


UPM/PARCS ALONE

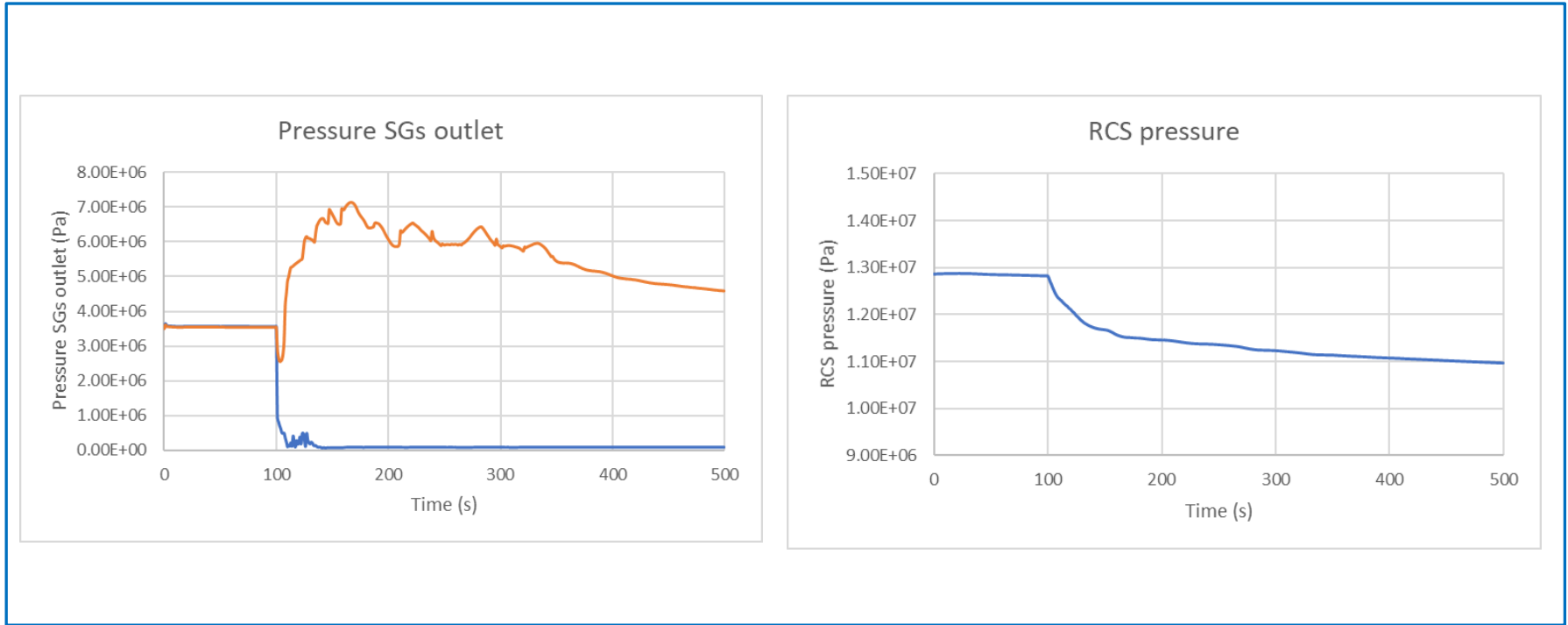


UPM/PARCS-TRACE

Axial Power Distribution



TRACE-1D/PARCS-3D model. Steam Line Break

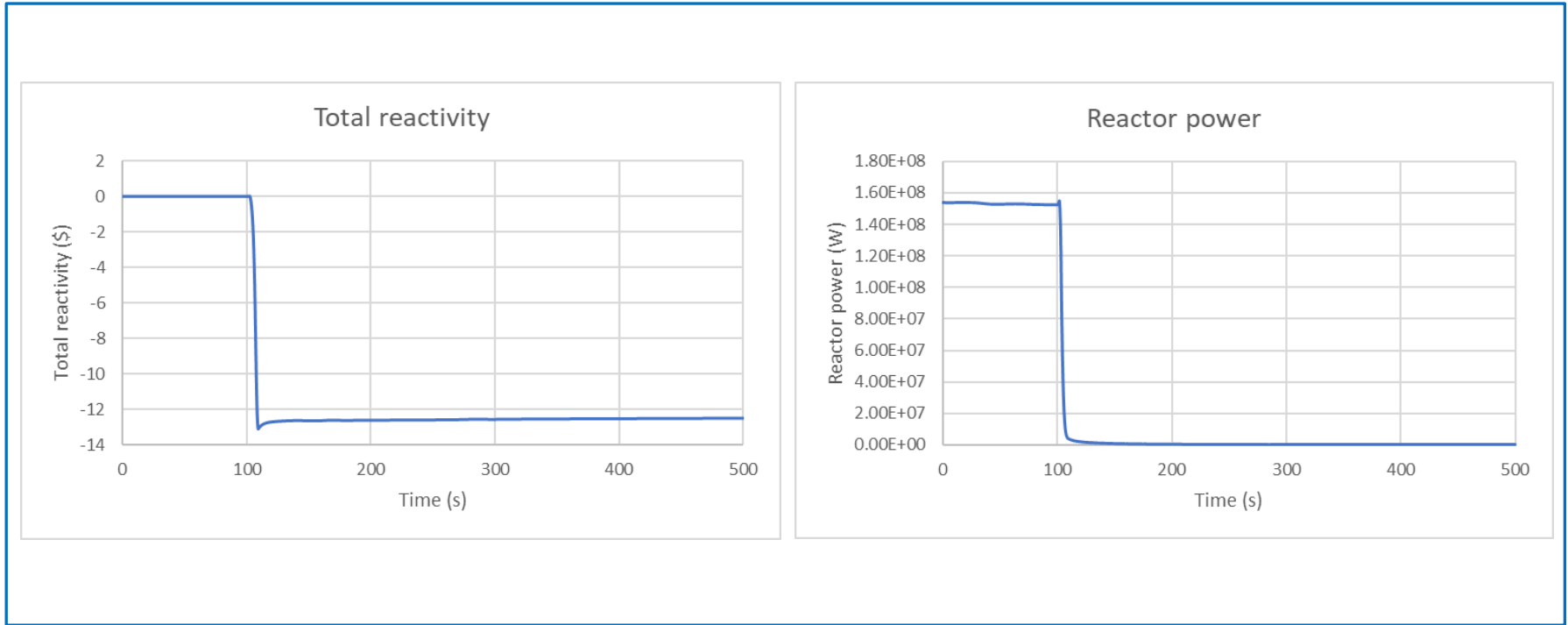


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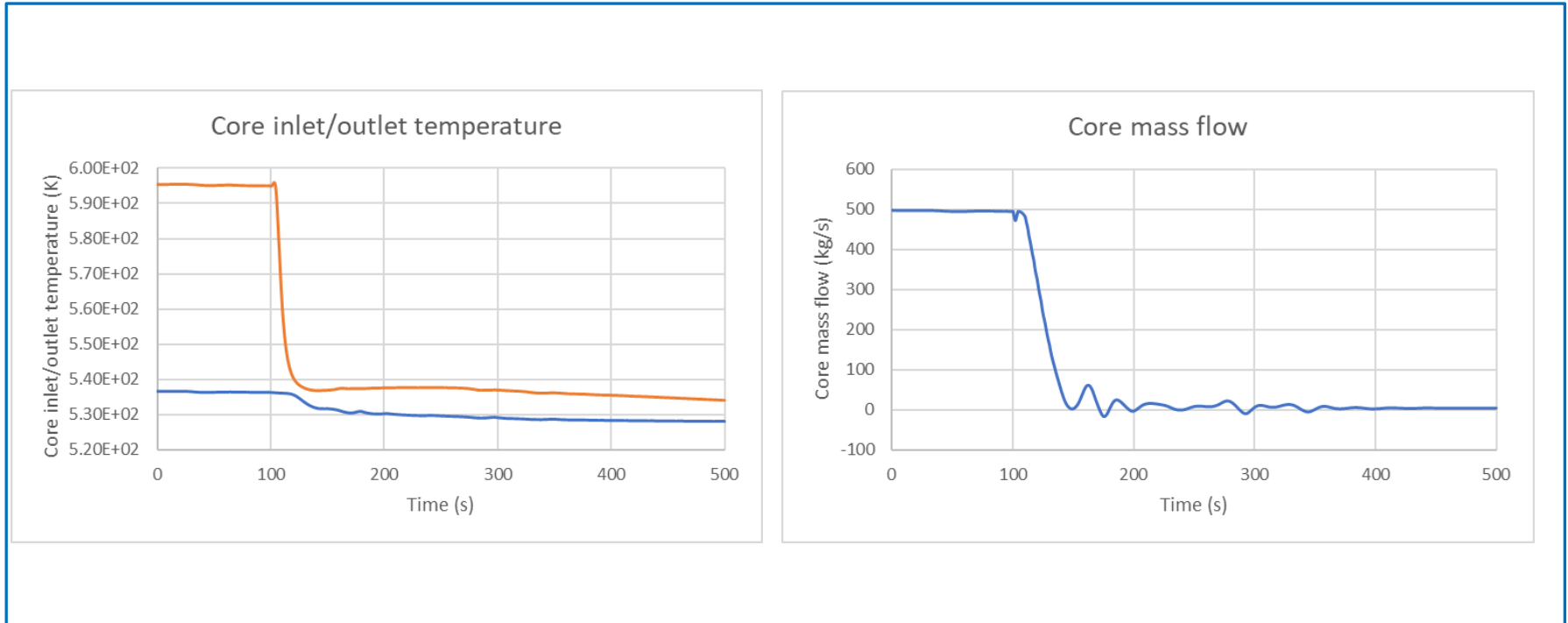


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TRACE-1D/PARCS-3D model. Steam Line Break



TRACE-1D/PARCS-3D model. Steam Line Break



Parameter	Nominal Value
Steam Line Break [s]	100
Low Steam Pressure setpoint [s]	103
SCRAM setpoint [-]	Low Steam Pressure setpoint
SCRAM signal [s]	103

Different numerical methods and convergence criteria are being tested:

- NEMG (4G),
- Hybrid (4G),
- FDM (2G).



CONCLUSIONS

- It has been obtained a NuScale representative model in PARCS. The model has then been validated with the results obtained from VTT's neutronic model.
- A Steam Break Line transient has been successfully simulated by coupling the core PARCS model with a TH plant model from TRACE code.
- PARCS is a suitable tool for the development of models for non-conventional reactors, such as NuScale.



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This work is part of the McSAFER project (IMPROVING SAFETY ANALYSIS METHODOLOGIES AND MOVING FROM TRADITIONAL TO HIGH-FIDELITY SAFETY ANALYSIS TOOLS FOR SMALL MODULAR REACTORS) that has received funding from the European Union's H2020/Euratom under grant agreement No. 945063

